

The International Academy for Production Engineering

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Overall indicators for comparing the performance of material extrusion printers with adaptive GBTA design

Laurent SPITAELS, Valentin DAMBLY, Édouard RIVIERE-LORPHEVRE and François DUCOBU

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On each part, more than :

- 400 dim. measurements
- 100 geo. <u>measurements</u>

If 5 parts printed on 10 printers → Huge dataset !



Presentation Plan

- 1. Context and Motivations
- 2. Method
- 3. Results
 - Dimensional performance
 - Geometrical performance
 - Overall performance
- 4. Conclusions and Future Research Opportunities

Printers evaluated

\rightarrow 3 MEX printers using filaments







Test artifact selection

- From literature and based itself on the NIST test artifact
- Adaptive design which can be fitted into any MEX printer with a build volume larger than 132 mm x 132 mm x 17 mm (X, Y and Z)
- Systematic coverage of all achievable dimensional size ranges of ISO 286-1



[Spitaels2022]

TIRPe 2024

Printers evaluated and their adapted GBTA designs



Х

Х

Y Ø

Ζ

 \odot

 $100 \ \mathrm{mm}$



Ultimaker S3



Intamsys FunMat HT

ABS



PLA





PLA





Parts manufacturing







Intamsys FunMat HT

ABS





Z

Y X

100 mm



PLA





ABS

Ultimaker S3

PLA

N% 5012



Resulting Dataset

8500 dimensional measurements and 2800 geometrical measurements











	$egin{array}{c} { m Ultimaker} \ 2+ \ { m PLA} \end{array}$	Ultimaker S3 ABS	Ultimaker S3 PLA	$\begin{array}{c} {\rm Funmat \ HT} \\ {\rm ABS} \end{array}$
Dimensional measurements	2170	1975	1975	2380
Geometrical measurements	705	685	685	725



$\blacksquare X \blacksquare Y \blacksquare Z \square Other$



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 $\blacksquare X \blacksquare Y \blacksquare Z \square Other$



Very complete but:

- Difficult to establish direct conclusions...
- Lack of overall view

 \rightarrow Introducing **overall indicators** is of prime interest and can solve this problem !



 $\blacksquare X \blacksquare Y \blacksquare Z \square Other$



Very complete but:

- Difficult to establish direct conclusions...
- Lack of overall view

 \rightarrow The data can be analyzed using the concepts of Trueness and Precision from ISO 5725-1:

- Mean value (trueness)
- Standard deviation between the different parts (precision)

╋

 Standard deviation between the different axes (axes homogeneity)

Trueness and Precision – ISO 5725





Trueness and Precision – ISO 5725











Post treatment of the data – Dimensional measurements

ISO 286-1 method relying on the number of tolerance unit n (dimensionless)

$$n = \frac{1000 \cdot |D_n - D_m|}{i}$$
$$i = 0.45 \cdot \sqrt[3]{D} + 0.001 \cdot D$$
$$D = \sqrt{D_1 \cdot D_2}$$

With:

- D_n the nominal dimension
- D_m the measurement
- *D*₁ and *D*₂ the lower and upper bound of the dimensional size range

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With:

- *D_n* the nominal dimension
- D_m the measurement
- *D*₁ and *D*₂ the lower and upper bound of the dimensional size range

Example:

- Measurement D_m = 29.430 mm while the nominal dimension D_n = 29.5 mm
- Size range: 18 mm \rightarrow 30 mm \rightarrow *i* = 1.307 μ m \rightarrow *n* = 54



Size range
[mm]
1-3
3-6
6-10
10-18
18—30
30-50
50-80
80-120
120-180
180-250



Post treatment of the data – Geometrical measurements

Same idea as for the dimensional measurements

 \rightarrow Making them dimensionless and independent of the feature dimension

 \rightarrow No method in the standards: proposal of a dimensionless number g

$$g = 1000 \cdot \frac{E_{dev}}{E_{dim}}$$

With:

- E_{dev} the measured deviation
- *E*_{dim} the main dimension of the measured element (def. from ISO 2768-2)

Example:

- Flatness deviation of 0.174 mm
- Plane of 50 mm x 50 mm \rightarrow g = 0.174/50 = 3.48

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Post treatment of the data – Grouping data

Dimensional data:

- By printer, material, size range and principal axis
- Ex. U2+ PLA 18 mm 30 mm X axis

Geometrical data:

- By printer, material, type and principal axis
- Ex. FHT ABS Flatness Z axis



Post treatment of the data – Computing indicators

For a given category:

- Trueness: mean $\rightarrow \mu_n$ and μ_g
- Precision: standard deviation $\rightarrow \sigma_n$ and σ_g
- Axis homogeneity: standard deviation between the axes X, Y and Z $\rightarrow \sigma_{n_{axes}}$ and $\sigma_{g_{axes}}$



Dimensional trueness, precision scores of the printers' X axis

Size	FI	ΤI	U2	2+	US	US3		S3
ranges	A	BS	PI	A	AF	\mathbf{BS}	PI	ЪA
[mm]	μ_n	σ_n	μ_n	σ_n	μ_n	σ_n	μ_n	σ_n
1–3	67	7 9	65	58	47	48	37	40
3-6	96	40	53	44	191	48	119	49
6-10	66	33	61	50	137	85	105	82
10 - 18	48	44	62	76	48	22	33	21
18 - 30	73	45	57	49	95	35	86	50
30 - 50	93	55	60	59	105	56	90	48
50 - 80	108	45	65	55	155	54	124	62
80-120	149	58	147	93	193	56	207	105
120 - 180	184	63	26	8	328	85	341	148
180 - 250	298	32	215	52	/	/	/	/
Trueness	118	/	81	/	144	/	127	/
Precision	/	49	/	54	/	54	/	67

Trueness of a printer = mean of its μ_n

Example:

• FHT ABS Trueness =
$$\frac{1182}{10}$$
 = 118



Dimensional trueness, precision scores of the printers' X axis

Size	FHT		U2	U2+		US3		S3
ranges	AI	BS	PL	A	AF	\mathbf{BS}	PI	ĹΑ
[mm]	μ_n	σ_n	μ_n	σ_n	$\mid \mu_n$	σ_n	μ_n	σ_n
1-3	67	79	65	58	47	48	37	40
3-6	96	40	53	44	191	48	119	49
6 - 10	66	33	61	50	137	85	105	82
10 - 18	48	44	62	76	48	22	33	21
18 - 30	73	45	57	49	95	35	86	50
30 - 50	93	55	60	59	105	56	90	48
50-80	108	45	65	55	155	54	124	62
80 - 120	149	58	147	93	193	56	207	105
120 - 180	184	63	26	8	328	85	341	148
180 - 250	298	32	215	52	/	/	/	/
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Example:

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Precision of a printer = mean of its σ_n

Example:

• FHT ABS Trueness =
$$\frac{494}{10}$$
 = 49

Dimensional axes homogeneity scores of the Funmat HT

Size ranges			μ_n		
[mm]	Х	Υ	Ζ	Other	$\sigma_{n,axes}$
1-3	67	90	121	64	26
3-6	96	125	207	209	57
6-10	66	79	145	279	98
10 - 18	48	62	262	81	100
18 - 30	73	87	386	130	147
30 - 50	93	110	/	/	12
50 - 80	108	124	/	/	11
80 - 120	149	178	/	206	29
120 - 180	184	200	/	/	11
180 - 250	298	338	/	/	28
		Axes	Home	geneity	52

Axes Homogeneity of a printer = mean of its σ_{n_jaxes}

Example:

• FHT ABS Axes homogeneity $=\frac{519}{10} = 52$





Indicator of Dimensional Performance (IDP)

		$\begin{array}{c} \rm FHT \\ \rm ABS \end{array}$	U2+ PLA	$\begin{array}{c} \rm US3\\ \rm ABS \end{array}$	US3 PLA
Trueness	X	118	81	144	127
	Y Z	$\frac{139}{224}$	$\frac{67}{164}$	$\frac{124}{120}$	$\frac{109}{134}$
	Other	162	107	163	137
Precision	Х	49	54	54	67
	Υ	56	52	86	84
	Ζ	184	120	108	116
	Other	49	28	57	59
Axes Home	0.	52	47	58	57
IDP	Trueness	643	419	551	507
	Precision Axes Homo.	$\frac{338}{52}$	$\begin{array}{c} 254 \\ 47 \end{array}$	$\frac{305}{58}$	$\frac{326}{57}$

Each IDP is a sum of the previous scores:

IDP Trueness FHT = sum of the FHT Trueness scores

→643 = 118+139+224+162



Indicator of Dimensional Performance (IDP)

		$\begin{array}{c} \rm FHT \\ \rm ABS \end{array}$	U2+PLA	US3 ABS	US3 PLA
Trueness	X Y Z	118 139 224	81 67 164	144 124 120	127 109 134
Procision	Other X	162	107 54	163	137 67
1 Tecision	Y Z	49 56 184	$52 \\ 120$	86 108	84 116
	Σ Other	49	$\frac{120}{28}$	$\frac{108}{57}$	59
Axes Home	Axes Homo.		47	58	57
IDP	Trueness Precision Axes Homo.	643 338 52	$419 \\ 254 \\ 47$	$551 \\ 305 \\ 58$	$507 \\ 326 \\ 57$

Each IDP is a sum of the previous scores:

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- IDP Precision and Axes Homogeneity followed the same principle



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Problem: different order of magnitude



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Axes Home).	52	47	58	57
IDP	Trueness	643	419	551	507
	Precision	338	254	305	326
	Axes Homo.	52	47	58	57
IDP_{norm}	Trueness	0.000	1.000	0.411	0.607
	Precision	0.000	1.000	0.393	0.143
	Axes Homo.	0.546	1.000	0.000	0.091

Each IDP is a sum of the previous scores:

- IDP Trueness FHT = sum of the FHT Trueness scores →643 = 118+139+224+162
- IDP Precision and Axes Homogenneity followed the same principle

Problem: different order of magnitude
→ Nomalization of the IDP following:

$$IDP_{norm} = \frac{IDP_{max} - IDP}{IDP_{max} - IDP_{min}}$$

Indicator of Geometrical Performance (IGP)



- Indicator based on the dimensionless number g:
 - $\mu_g \rightarrow \text{Trueness}$
 - $\sigma_g \rightarrow \text{Precision}$
 - $\sigma_{g_axes} \rightarrow$ Axes Homogeneity
- Normalization, as before, to have the same order of magnitude and allow comparisons

$$IGP_{norm} = \frac{IGP_{max} - IGP}{IGP_{max} - IGP_{min}}$$

	Printer Material	$\begin{array}{c} \rm FHT \\ \rm ABS \end{array}$	U2+ PLA	$\begin{array}{c} \mathrm{US3} \\ \mathrm{ABS} \end{array}$	US3 PLA
Trueness	Х	1.671	2.804	3.365	2.598
	Υ	1.275	2.695	5.229	3.918
	Z	2.088	2.153	1.960	1.941
	Other	8.392	10.243	8.051	8.550
Precision	Х	1.220	1.137	2.279	1.380
	Υ	0.781	1.080	4.648	2.164
	Z	0.824	1.153	1.019	1.157
	Other	6.358	7.116	6.542	5.494
Axes Home	0.	0.274	1.187	1.901	1.212
IGP	Trueness	13.426	17.895	18.605	17.007
	Precision	9.183	10.486	14.488	10.195
	Axes Homo.	0.274	1.187	1.901	1.212
IGP_{norm}	Trueness	1.000	0.137	0.000	0.308
	Precision	1.000	0.754	0.000	0.809
	Axes Homo.	1.000	0.439	0.000	0.423



Overall Perfomance Indicators (OPI)

Averaging the normalized IDP and IGP:

- Obtain the OPI;
- Gives the same weight to dimensional and geometrical scores;
- Can be displayed as a radar graph to ease the read.

	Printer Material	$\begin{array}{c} \mathrm{FHT} \\ \mathrm{ABS} \end{array}$	U2+PLA	US3 ABS	US3 PLA
OPI	Trueness	0.500	0.568	0.206	0.458
	Precision	0.500	0.877	0.197	0.476
	Axes Homo.	0.773	0.719	0.000	0.257



Context | Method | Results | Conclusions and Outlook

Results

Overall Perfomance Indicators (OPI)

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Overall Performance Indicator (OPI)

Conclusions

- The Ultimaker 2+ using PLA exhibited the best overall performance with the highest trueness and precision.
- The Funmat HT exhibited the best axes homogeneity.
- The Ultimaker S3 showed better performance using PLA than ABS
- \rightarrow Significant influence of the material choice on the measured performance.



Overall Performance Indicator (OPI)



Conclusions

- The concepts of trueness, precision and axes homogeneity were used to rank the the tested printers.
- The OPI gives an image of the overall dimensional and geometrical performance in a single indicator.
- Precautions should be taken using the OPI since it can hide under performance that can be detected using the IDP and IGP.
- The identical weights given to the *IDP* and *IGP* performance for the computation of the *OPI* could be tuned.



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Future Research Opportunities

 Measuring axis backlash and positioning repeatability to confirm the better performance of the Funmat HT and Ultimaker 2+ in terms of axes homogeneity.

 Quantifying the improvement of a printer after its modifications (firmware update for the axes stepper calibration, new printing parameters, *e.g.*) or compensation by using the proposed indicators.

 Adding other contributions into the OPI, such as the specific energy consumption could be interesting to evaluate the performance of the printers more comprehensively.





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Context



NAS 979 for machining centers



NIST Test artifact for AM printers



Square base: 100 mm x 100 mm

Square base: 100 mm x 100 mm

Test artifact selection

- From literature and based itself on the NIST test artifact
- Adaptive design which can be fitted into any MEX printer with a build volume larger than 132 mm x 132 mm x 17 mm (X, Y and Z)
- Systematic coverage of all achievable dimensional size ranges of ISO 286-1





Test artifact selection

- From literature and based itself on the NIST test artifact
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Context

Off-machine metrology

Measuring the part after its fabrication

Advantages:

- Non-invasive for the machine
- Affordable
- Conventional means (CMM, *e.g.*)) can be used for the parts measurement
- Comparison of several machines possible and eased

Disadvantages:

- No direct link between a deviation and its cause
- Design of the part conditioned by the measuring device foreseen

Adapted for the industrial context with limited measuring means and machine modifications
 Already used since decades for the performance assessment of machining center (NAS 979)

-

-



Parameters	Units	Ultimaker 2+ (U2+)	Ultimaker S3 (US3)	Funmat HT (FHT)
Build volume (XYZ)	[mm]	$223 \times 223 \times 205$	$230 \times 190 \times 200$	$243 \times 243 \times 260$
Feedstock	/	ø 2.85 mm Filaments	ø 2.85 mm Filaments	ø 1.75 mm Filaments
Nozzle temperature	[°C]	220 (PLA)	215 (PLA), 240 (ABS)	255 (ABS)
Build platform temperature	[°C]	60 (PLA)	60 (PLA), 85 (ABS)	85 (ABS)
Nozzle diameter	[mm]	0.4	0.4	0.4
Layer thickness	[mm]	0.1	0.1	0.1
Infill density	[%]	20	20	20
Infill pattern	/	Cubic	Cubic	Cubic
Brim	[mm]	8	8	8
Print time	[h]	30	24 (PLA), 29 (ABS)	54





Parameters Units		Ultimaker 2+ (U2+)	Ultimaker S3 (US3) Funmat HT		T (FHT)
Build volume (XYZ) [mm] Feedstock /		$223 \times 223 \times 205$ ø 2 85 mm Filaments	$230 \times 190 \times 200$ ø 2.85 mm Filaments	243×243 ø 1 75 mm	× 260 n Filaments
Nozzle temperature	[°C]	220 (PLA)	215 (PLA), 240 (ABS)	255 (ABS))
Build platform temperature	[°C]	60 (PLA)	60 (PLA), 85 (ABS)	85 (ABS)	
Nozzle diameter	[mm]	0.4	0.4	0.4	
Layer thickness	[mm]	0.1	0.1	0.1	Common printing
Infill density	[%]	20	20	20	paramotors
Infill pattern	/	Cubic	Cubic	Cubic	parameters
Brim	[mm]	8	8	8	
Print time	[h]	30	24 (PLA), 29 (ABS)	54	



Measurement of the parts

- CMM Wenzel LH 54 with a PH10M Renishaw Head
- Probe diameter: 1.5 mm
- Part and skirt removed from the build platform

Geometrical features	Number of probed points
Cylinders	8 distributed over 2 circles
Hemispheres	9 distributed over 3 circles
Planes in general	6
Top planes	39 (U2+), 40 (US3) and 47 (FHT)





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Geometrical trueness, precision and axes homogeneity scores

Type of measurement	Axis	$\begin{array}{c} \mathrm{FHT} \\ \mathrm{ABS} \end{array}$	U2+PLA	$\begin{array}{c} \rm US3\\ \rm ABS \end{array}$	US3 PLA
Cylindricity	Other	10.464	12.420	11.121	13.222
Flatness	X Y	$1.056 \\ 0.594$	$0.435 \\ 0.864$	$2.257 \\ 3.585$	$1.115 \\ 2.191$
	\mathbf{Z} Other	$1.547 \\ 1.132$	$1.461 \\ 2.572$	$1.893 \\ 0.874$	$\begin{array}{c} 1.843 \\ 1.931 \end{array}$
Parallelism	X Y Z Other	3.526 2.873 2.629 3.081	7.803 7.027 2.845 2.979	$7.633 \\ 11.945 \\ 2.026 \\ 3.110$	$6.189 \\ 9.267 \\ 2.039 \\ 4.498$
Profile	Other	22.813	26.981	16.223	13.673
Perpendicularity	Other	4.470	6.266	8.927	9.426
Straightness	X Y	$0.430 \\ 0.359$	$0.174 \\ 0.195$	$0.205 \\ 0.156$	$0.491 \\ 0.295$

Mean value of $g: \mu_g$



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	Printer Material	$_{ m ABS}$	U2+PLA	$\begin{array}{c} \rm US3 \\ \rm ABS \end{array}$	US3 PLA
Trueness	X Y Z Other	$ \begin{array}{r} 1.671 \\ 1.275 \\ 2.088 \\ 8.392 \end{array} $	$2.804 \\ 2.695 \\ 2.153 \\ 10.243$	$3.365 \\ 5.229 \\ 1.960 \\ 8.051$	$2.598 \\ 3.918 \\ 1.941 \\ 8.550$
Precision	X Y Z Other	$\begin{array}{c} 1.220 \\ 0.781 \\ 0.824 \\ 6.358 \end{array}$	$\begin{array}{c} 1.137 \\ 1.080 \\ 1.153 \\ 7.116 \end{array}$	$\begin{array}{c} 2.279 \\ 4.648 \\ 1.019 \\ 6.542 \end{array}$	$\begin{array}{c} 1.380 \\ 2.164 \\ 1.157 \\ 5.494 \end{array}$
Axes Home	0.	0.274	1.187	1.901	1.212

 \rightarrow Same principle as before,

 \rightarrow Idem for precison and axes homogeneity

Mean value of $g: \mu_g$

Indicator of Geometrical Performance (IGP)

Each IGP is a sum of the previous scores:

IGP Trueness FHT = sum of the FHT Trueness scores

→13.426 = 1.671 + 1.275 + 2.088 + 8.392

 IGP Precision and Axes Homogenneity followed the same principle

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Each IGP is a sum of the previous scores:

IGP Trueness FHT = sum of the FHT Trueness scores

→13.426 = 1.671 + 1.275 + 2.088 + 8.392

- IGP Precision and Axes Homogenneity followed the same principle
- → Normalization, as before, to have the same order of magnitude and allow comparisons

$$IGP_{norm} = \frac{IGP_{max} - IGP}{IGP_{max} - IGP_{min}}$$

	Printer Material	$\begin{array}{c} \mathrm{FHT} \\ \mathrm{ABS} \end{array}$	U2+PLA	$\begin{array}{c} \mathrm{US3} \\ \mathrm{ABS} \end{array}$	US3 PLA
Trueness	Х	1.671	2.804	3.365	2.598
	Υ	1.275	2.695	5.229	3.918
	Z	2.088	2.153	1.960	1.941
	Other	8.392	10.243	8.051	8.550
Precision	Х	1.220	1.137	2.279	1.380
	Υ	0.781	1.080	4.648	2.164
	\mathbf{Z}	0.824	1.153	1.019	1.157
	Other	6.358	7.116	6.542	5.494
Axes Homo.		0.274	1.187	1.901	1.212
IGP	Trueness	13.426	17.895	18.605	17.007
	Precision	9.183	10.486	14.488	10.195
	Axes Homo.	0.274	1.187	1.901	1.212
IGPnorm	Trueness	1.000	0.137	0.000	0.308
	Precision	1.000	0.754	0.000	0.809
	Axes Homo.	1.000	0.439	0.000	0.423

